

# The CodeRed experiments - Evidence based fire safety solutions for timber buildings

Enabling safe and sustainable buildings

# Mass timber construction

Increasing demand by governments, developers, suppliers

## DRIVEN BY:

- Climate crisis  
*Desire to reduce the embodied carbon in buildings and infrastructure*
- Speed of construction
- Cost savings
- Architectural aspirations

900,000 kilograms of CO<sub>2</sub> saved through building Origine, Québec City, in timber rather than conventional materials

49 weeks to complete Stadhaus, London in mass timber compared to 72 weeks for equivalent concrete buildings





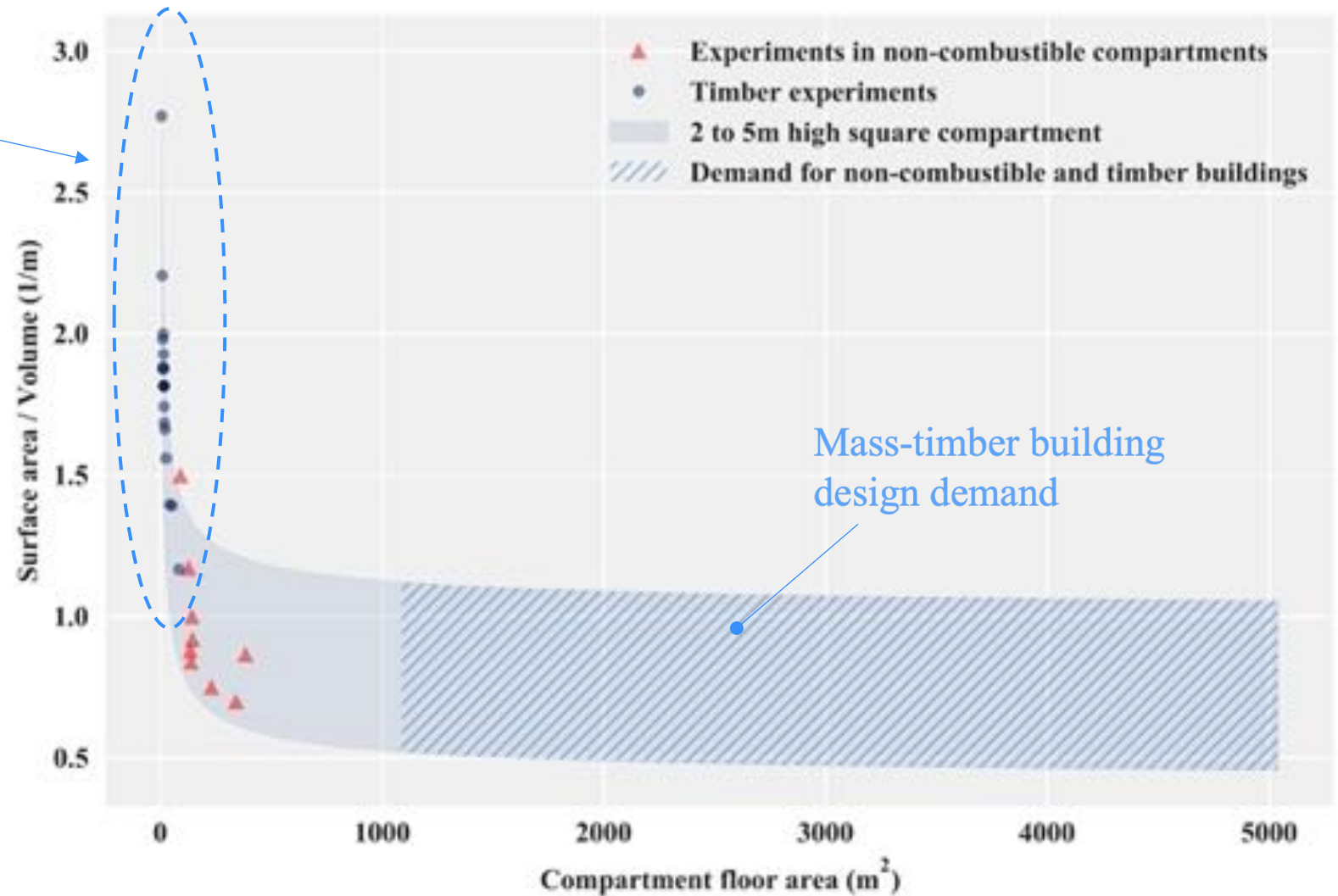
### The challenge

Evidencing that the use of timber at scale can be safe

# Current Knowledge

Observations in fire tests with exposed CLT

Previous timber experiments  
limited to compartments of  
under 90 m<sup>2</sup>





## Letter to the Editor: Design Fires for Open-Plan Buildings with Exposed Mass-Timber Ceiling

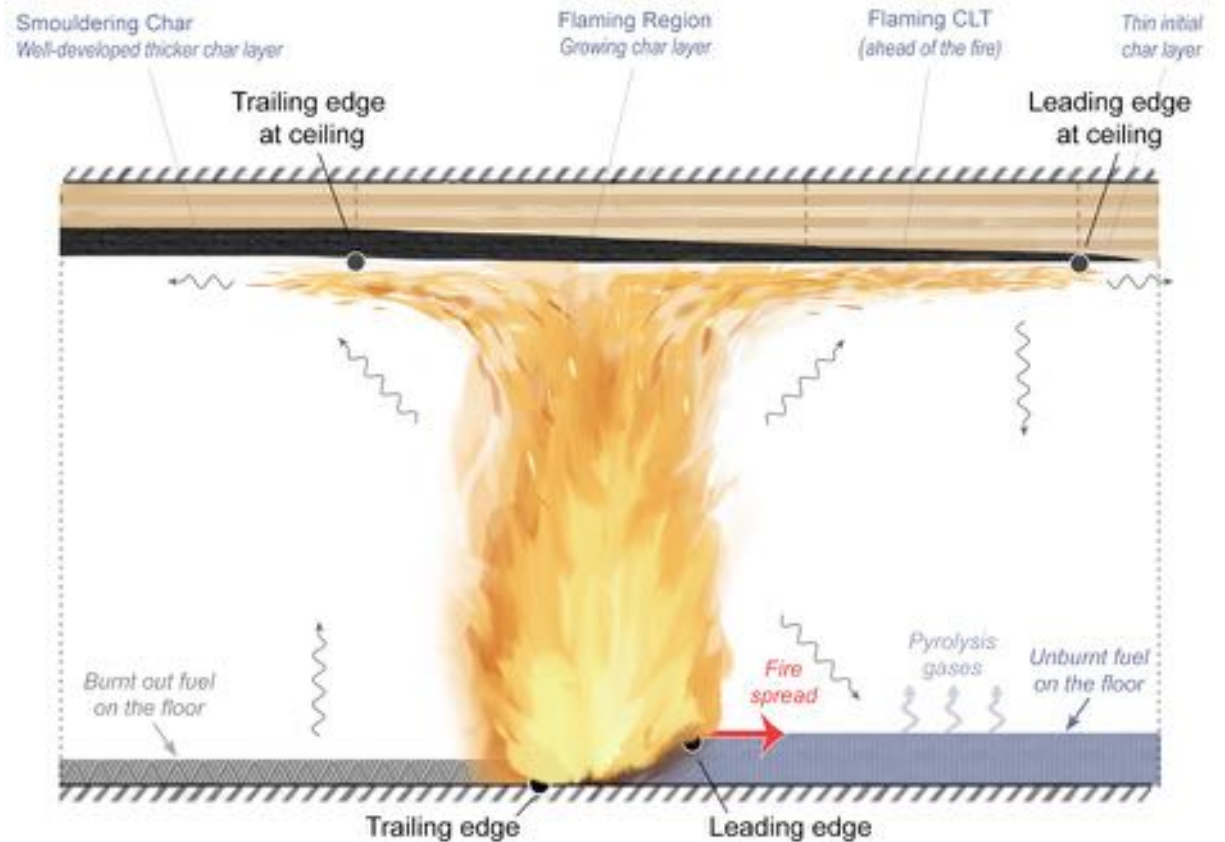
Egle Rockauskaite, Arup, London, UK  
Panagiotis Kotsovinos\*, Arup, Manchester, UK  
David Barber, Arup, Washington, DC, USA

Dear editor,

Over the past decade, the design and construction of mass timber buildings using cross laminated timber (CLT) and glulam have significantly increased globally. This is mainly due to the benefits of timber construction in the global fight against climate change and a decarbonised economy. In addition, it meets architectural aspirations, can result in a reduced cost and improved speed of construction, in comparison to conventional, typically non-combustible construction forms. Many recent proposals by architects include high-rise mass timber buildings for office and public uses with large open-plan floor areas that are greater than 1000 m<sup>2</sup> with aspirations of maintaining as much timber exposed as possible.

For the structural fire design of high-rise buildings, a key issue to be addressed is the requirement for the building to withstand burn-out of a fully developed fire. When the load-bearing member is combustible and is exposed there is a feedback loop between the fire severity and structural response (through timber charring) resulting in more onerous fire conditions. The uncertainty of the types of fires that are therefore likely to occur in large-open plan compartments with exposed load-bearing timber, and how the timber may contribute to the fire, is a complex area that has not received enough attention from regulators, standardisation bodies, the industry or the research community.

A conservative measure to mitigate the inherent risk combustible load-bearing



- Fire design methodologies have been developed based on 84m<sup>2</sup> compartments and → *require further validation for large compartments*
- Travelling fires methodology not developed for application to timber structures
- Knowledge gaps and research needs to apply travelling fires to timber

# CodeRed

Large scale CLT fire  
experiments

# CodeRed

## Research aims

### SEEK TO UNDERSTAND:

1. The **effect of exposed timber on fire dynamics** in large open-plan compartments
2. The **decay behaviour** of exposed mass timber surfaces
3. How **observed fires compare to the standard fire exposure** (e.g. time-equivalence)
4. The **travelling fire spread rates** in large compartments when lined with timber construction
5. The **charring rates in natural fires** as a function of received radiation

### CodeRed #02:

1. The **effect of reduced ventilation (50%)** in large open-plan compartments with exposed timber

### CodeRed #04 :

1. The **effect of encapsulation (50%)** in large open-plan compartments with exposed timber



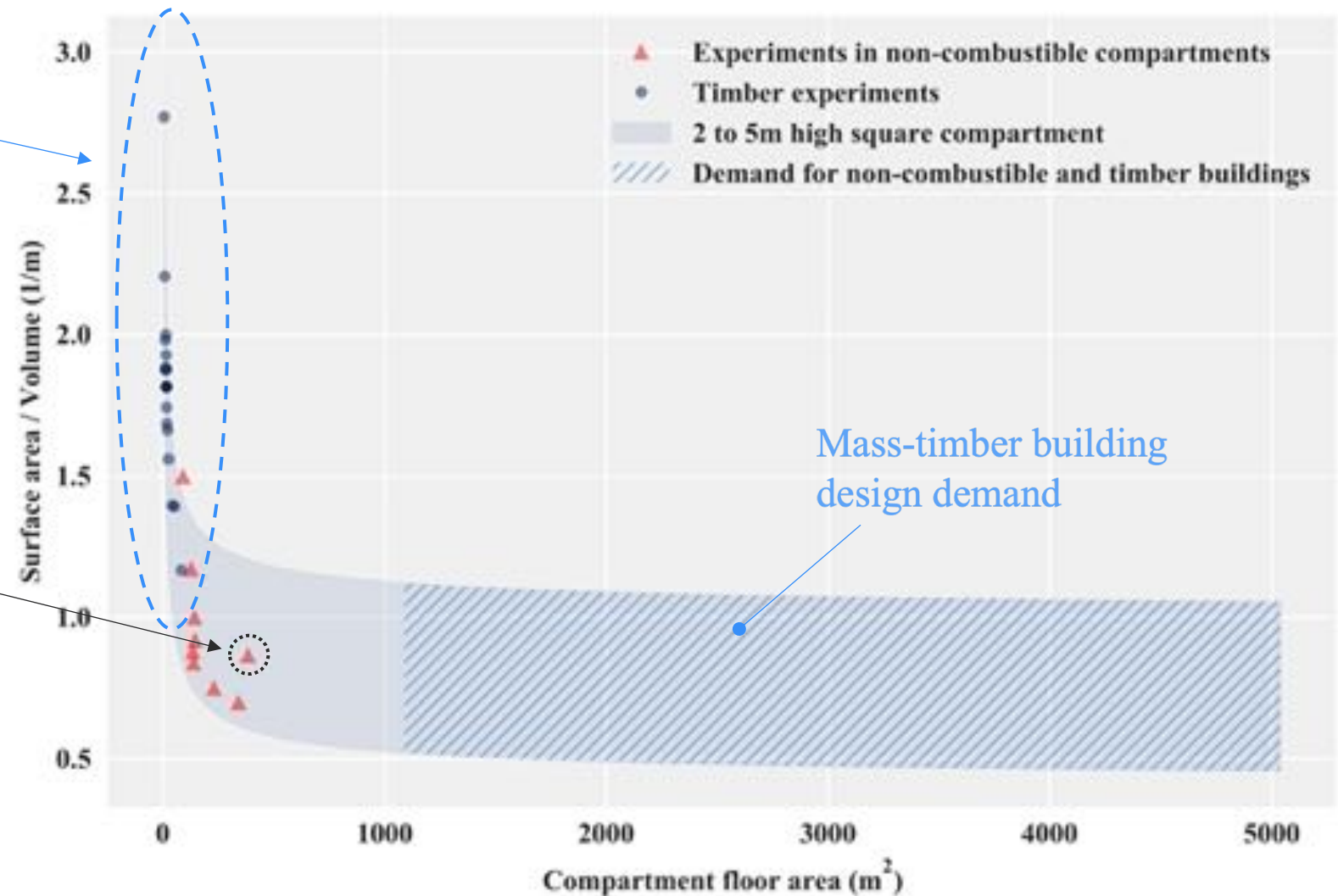
# Previous travelling fire experiments

Observations in fire tests with exposed CLT

Previous timber experiments limited to compartments of under 90 m<sup>2</sup>

x-ONE & x-TWO

Largest fire experiments in terms of compartment floor area (~380m<sup>2</sup>) conducted to date worldwide



Mass-timber building design demand



# Steering Group

Close academic and industry collaboration with oversight by steering group, and input from project application



Fabienne Robert

CERIB Project Director  
Fire Test House



David Barber

Global timber fire safety  
lead, EC5 committee



Prof. Andrew Lawrence

Steering Group –  
structural timber expert,  
EC5 committee



Prof. Guillermo Rein

Steering Group – ICL fire  
dynamics, smouldering  
expert



Alistair Murray

Steering Group – Arup  
Fire UK Leader



Dr. Clare Perkins

Steering Group –  
materials expert



Dr. Susan Lamont

Steering Group – global  
fire skills lead



Eoin O'Loughlin

Steering Group – global  
structural fire skills lead



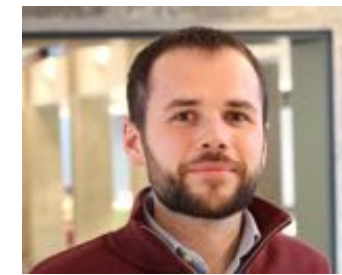
Harry Mitchell

Steering Group – PhD  
student, ICL



Rikesh Amin

Steering Group – PhD  
student, ICL



Daniel Thomson

Fire UK Timber skills  
lead

# The building

Experimental layout for CodeRed

- 352 m<sup>2</sup> | 10.27 m wide, 34.27 m long, 3.1 m high



# The building

Experimental layout for CodeRed

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- CLT ceiling comprises 5-ply CLT with MUF adhesive
- Two timber columns (glulam)
- One protected steel column

# The building

Experimental layout for CodeRed

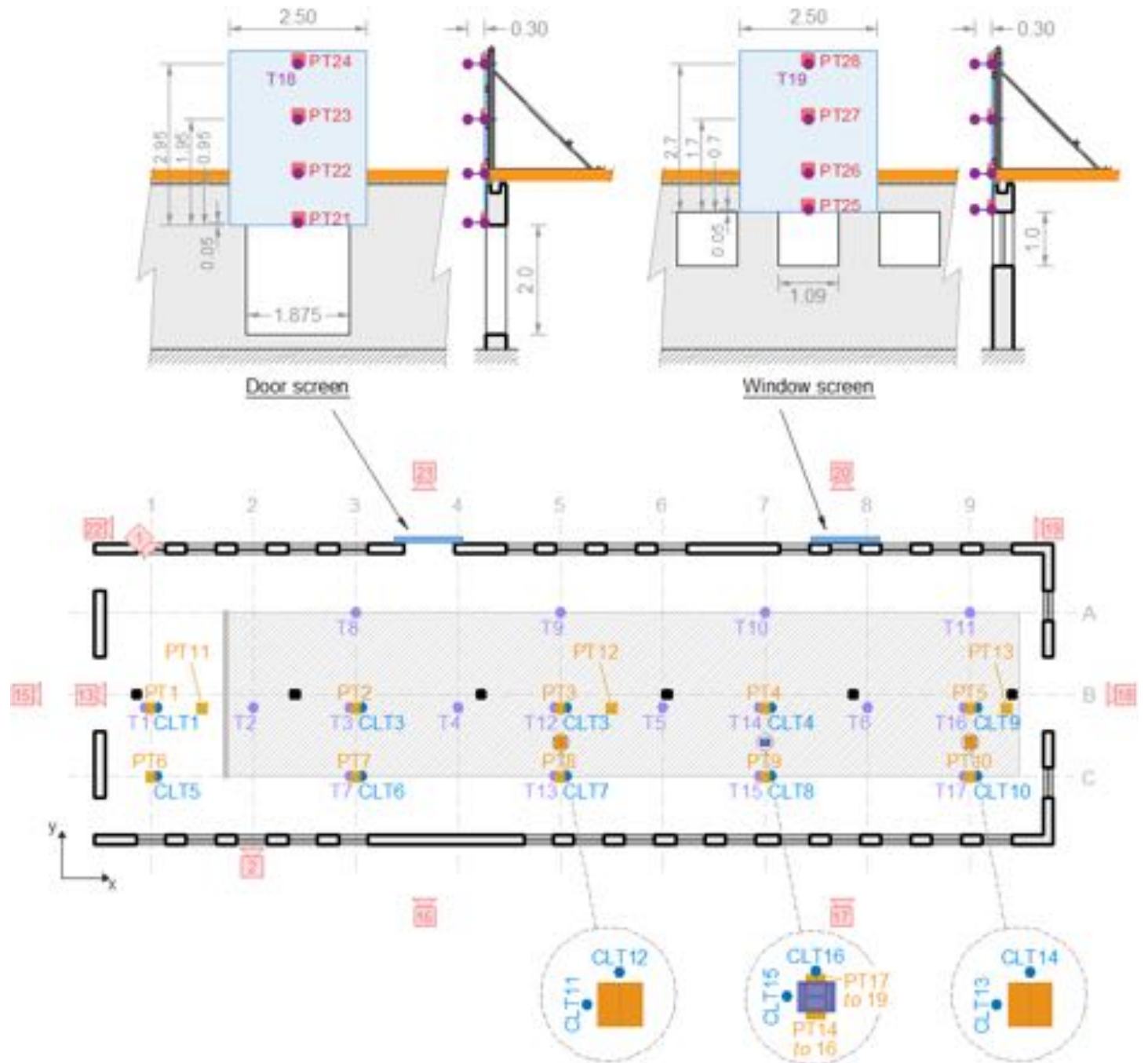
- $\sim 370 \text{ MJ/m}^2$  wood crib



# Instrumentation

CodeRed #01 shown indicatively

- **PT - plate thermocouples**
  - PT1 to 13: 100mm below the ceiling
  - PT14 to 19: 100mm from the steel column at 100, 700 & 2100mm below the ceiling
  - PT21 to 28: fixed to the external screens
- **CLT - Type-K thermocouples within CLT panels**
  - CLT1 to 16: embedded 20, 40, 60 & 80 mm from the exposed surface
- **T - Type-K thermocouple trees**
  - T1 to 11: 100, 700 & 2100 mm below the ceiling
  - T2 to 17: 100, 700, 2100 & 2800 mm below the ceiling
  - T18 to 19: 0 and 300 mm from the external screens



# The CodeRed experiment series (2021)

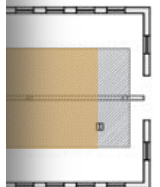
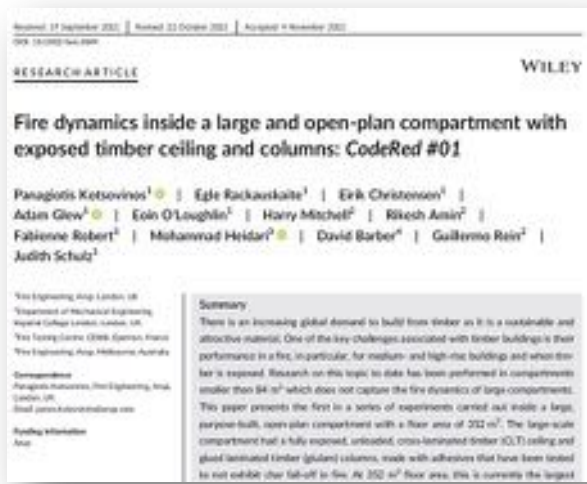


JP

Localised water mist system test

	CodeRed #01	CodeRed #02	CodeRed #03	CodeRed #04
Ventilation	21%	10%	10%	21%
Encapsulation	none	none	none	50%

Publication in progress



encapsulation

# CodeRed #01

*Impact of adding CLT*

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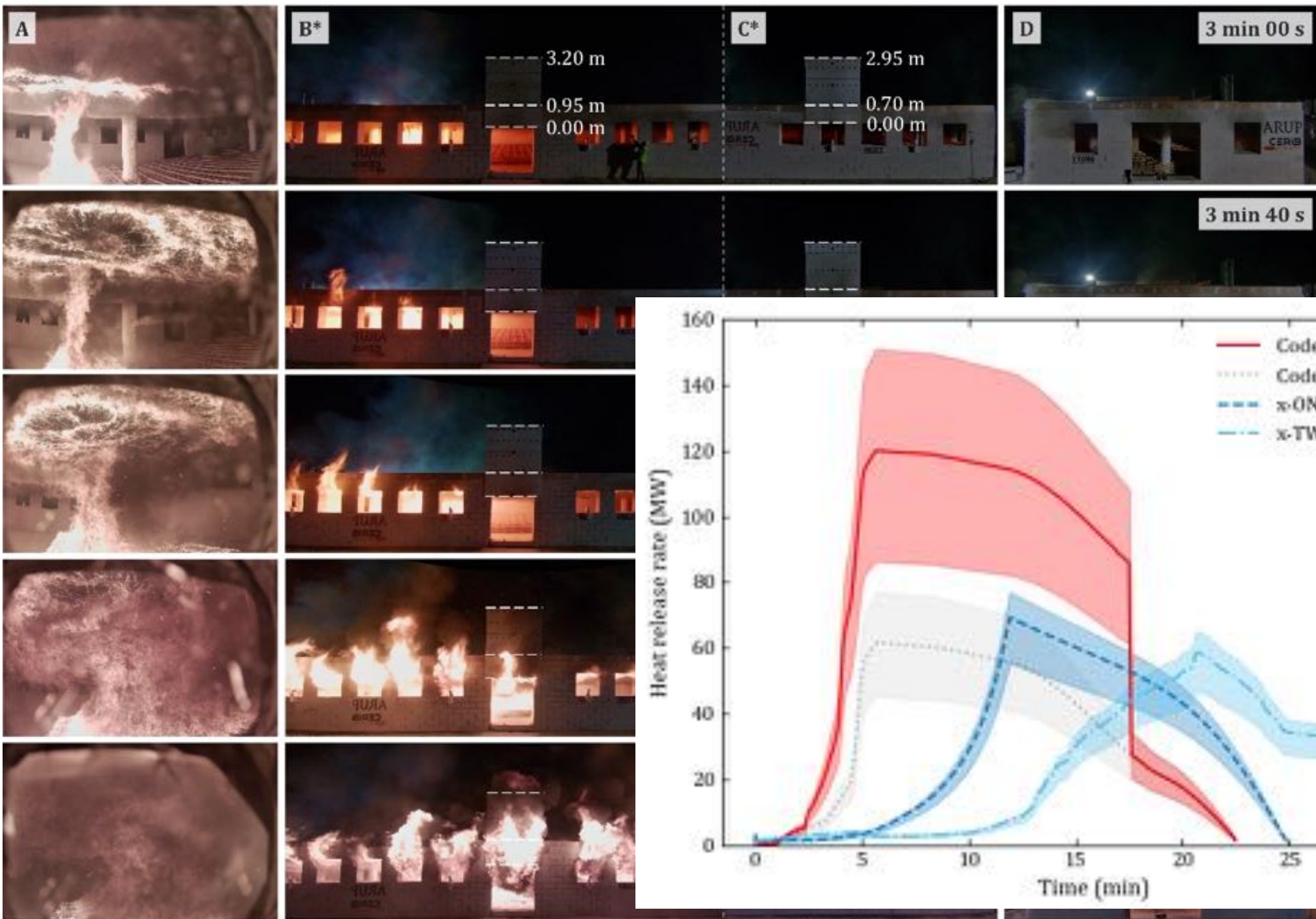
CERUB

Fire Testing Centre



~1.5 min





~6 min



AM – 10<sup>th</sup> March



AM – 10<sup>th</sup> March



# Smouldering

CodeRed #01

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t = 3.18 h

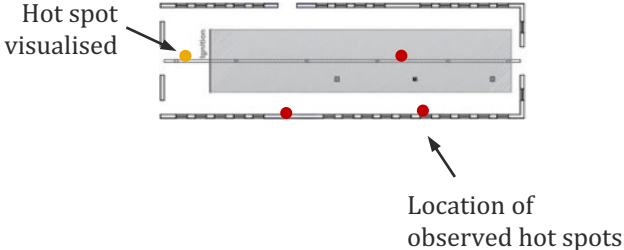
t = 14.28 h

t = 38.08 h

Infrared






Visual



RESEARCH ARTICLE

WILEY

# Fire dynamics inside a large and open-plan compartment with exposed timber ceiling and columns: *CodeRed #01*

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Adam Glew<sup>1</sup>  | Eoin O'Loughlin<sup>1</sup> | Harry Mitchell<sup>2</sup> | Rikesh Amin<sup>2</sup> |  
Fabienne Robert<sup>3</sup> | Mohammad Heidari<sup>3</sup>  | David Barber<sup>4</sup> | Guillermo Rein<sup>2</sup> |  
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## Correspondence

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## Funding information

Arup

## Summary

There is an increasing global demand to build from timber as it is a sustainable and attractive material. One of the key challenges associated with timber buildings is their performance in a fire, in particular, for medium- and high-rise buildings and when timber is exposed. Research on this topic to date has been performed in compartments smaller than 84 m<sup>2</sup> which does not capture the fire dynamics of large compartments. This paper presents the first in a series of experiments carried out inside a large, purpose-built, open-plan compartment with a floor area of 352 m<sup>2</sup>. The large-scale compartment had a fully exposed, unloaded, cross-laminated timber (CLT) ceiling and glued laminated timber (glulam) columns, made with adhesives that have been tested to not exhibit char fall-off in fire. At 352 m<sup>2</sup> floor area, this is currently the largest

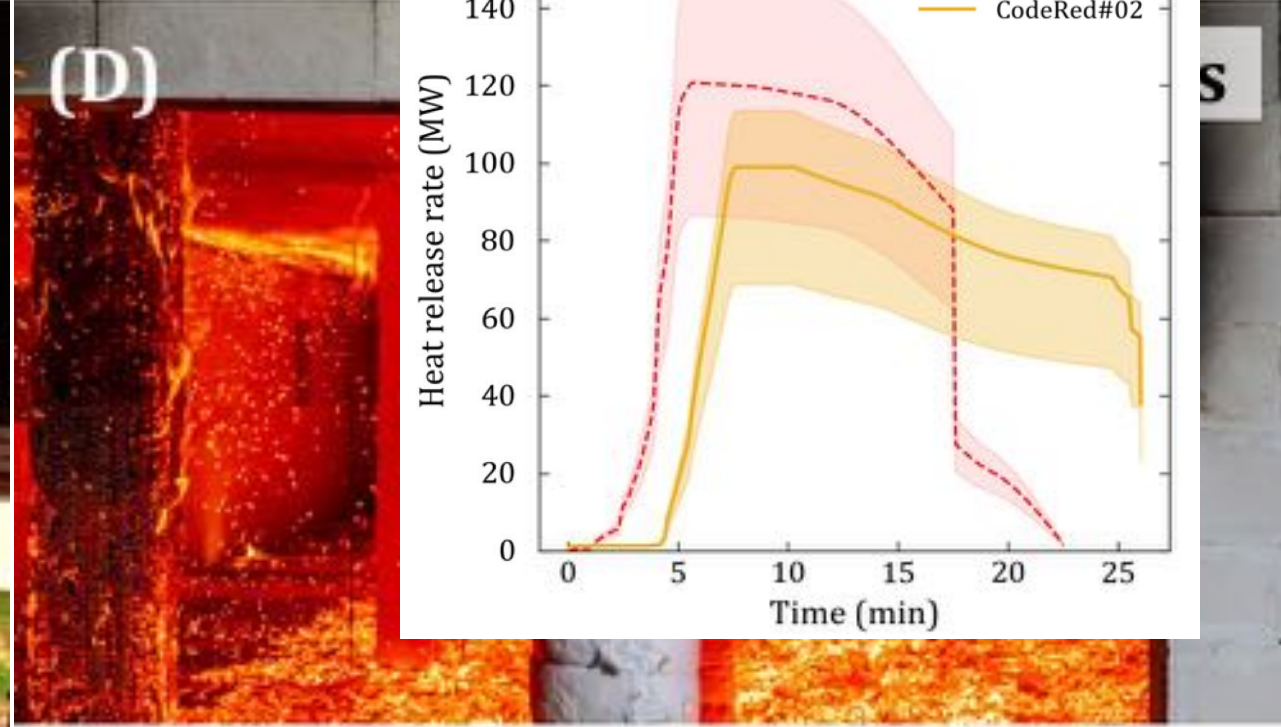
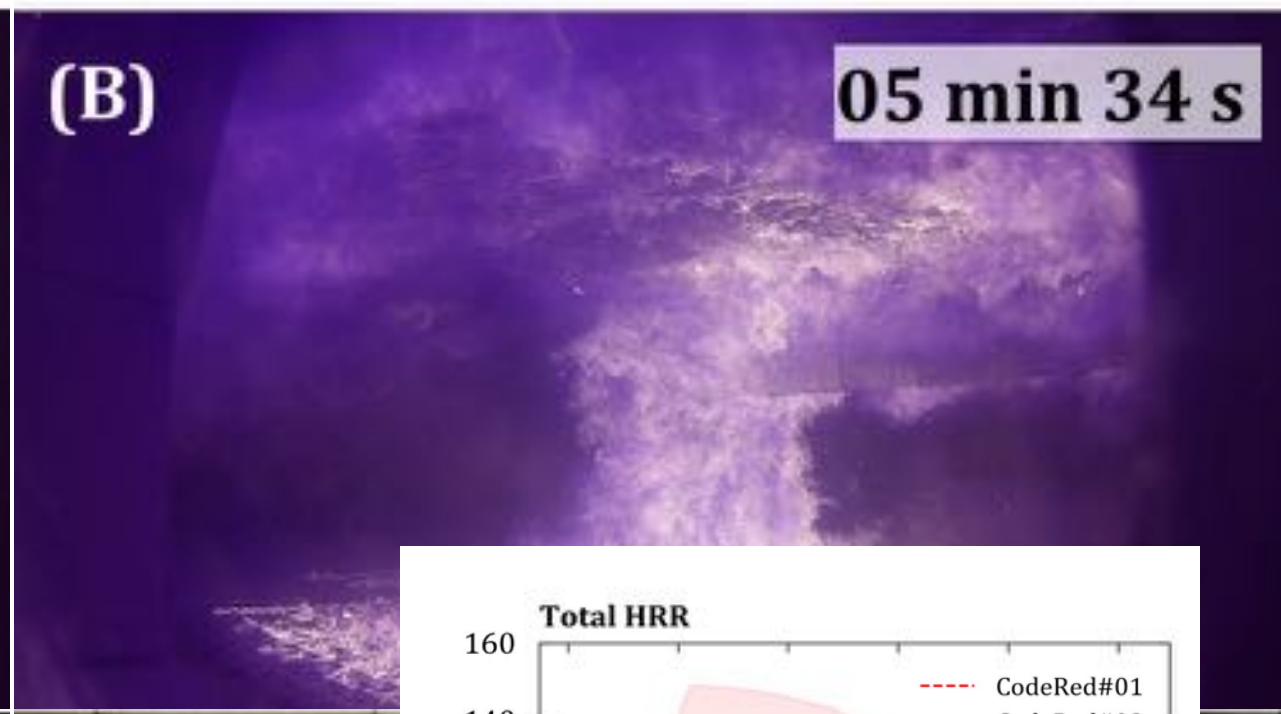
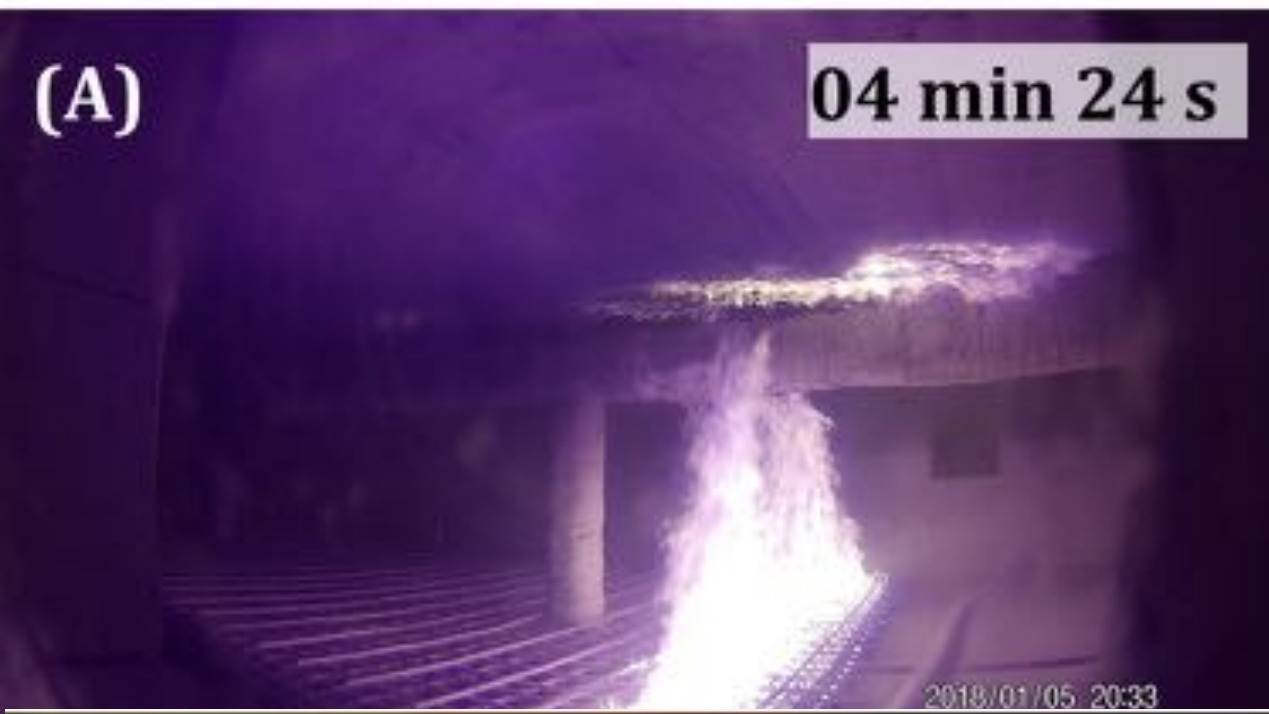
# CodeRed #02

*Impact of reduced ventilation*



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# External flaming



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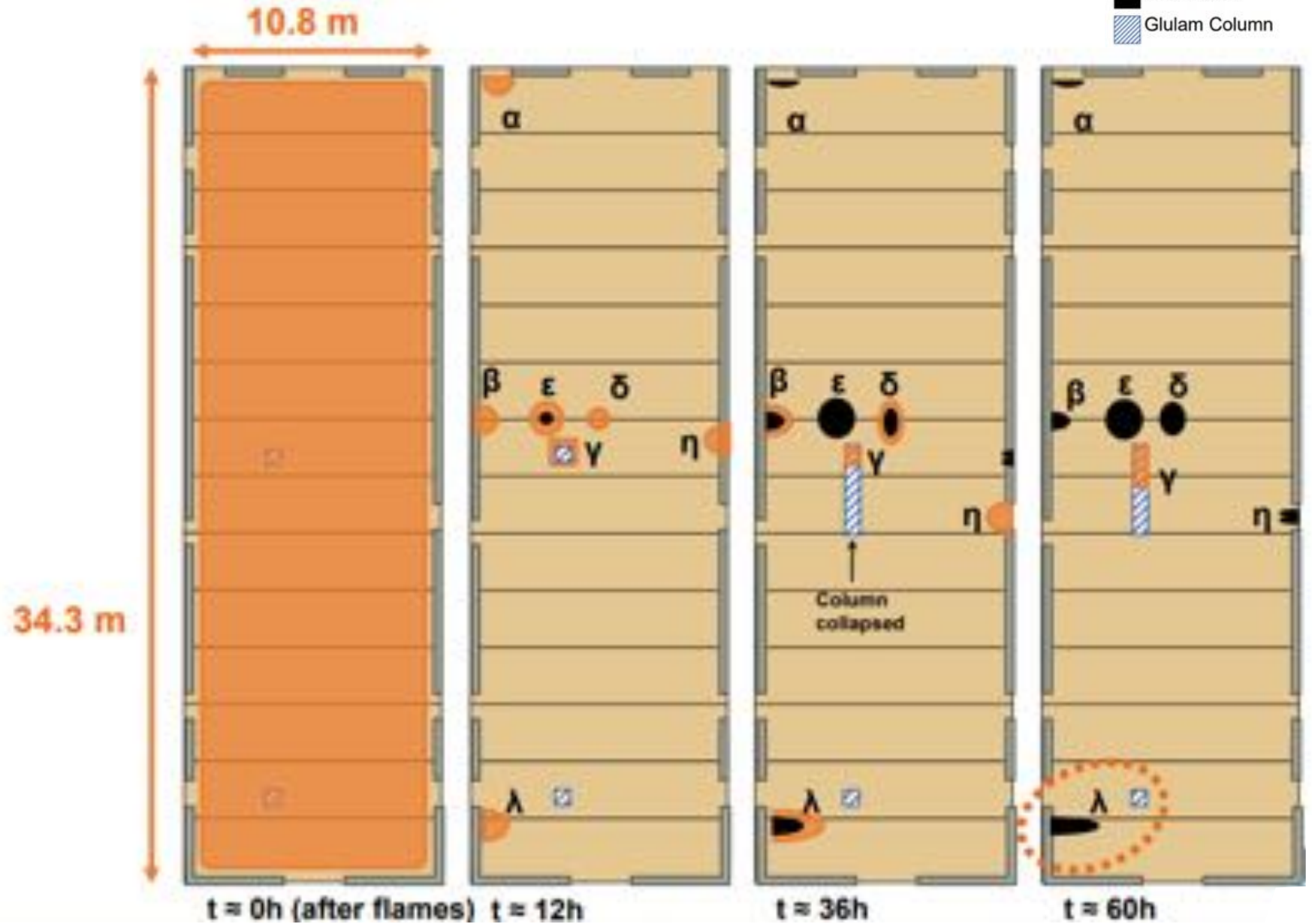


- Slightly **greater external flaming** height than CR #01;  
*3 to 3.5 m in height*
- Much 'smokier' (incomplete combustion)
- Pulsating flames
- Large lateral flame extensions

# Smouldering

CodeRed #02

- CLT ceiling
- Hotspot
- Hole in CLT
- Glulam Column



Mitchell, H., Amin, R., Kotsovinos, P., and Rein, G. (2022), *Structural Hazards of Smouldering in Tall Timber Buildings*, SFPE Annual Conference, Detroit

Imperial College  
London

## RESEARCH ARTICLE

WILEY

# Impact of ventilation on the fire dynamics of an open-plan compartment with exposed timber ceiling and columns: *CodeRed #02*

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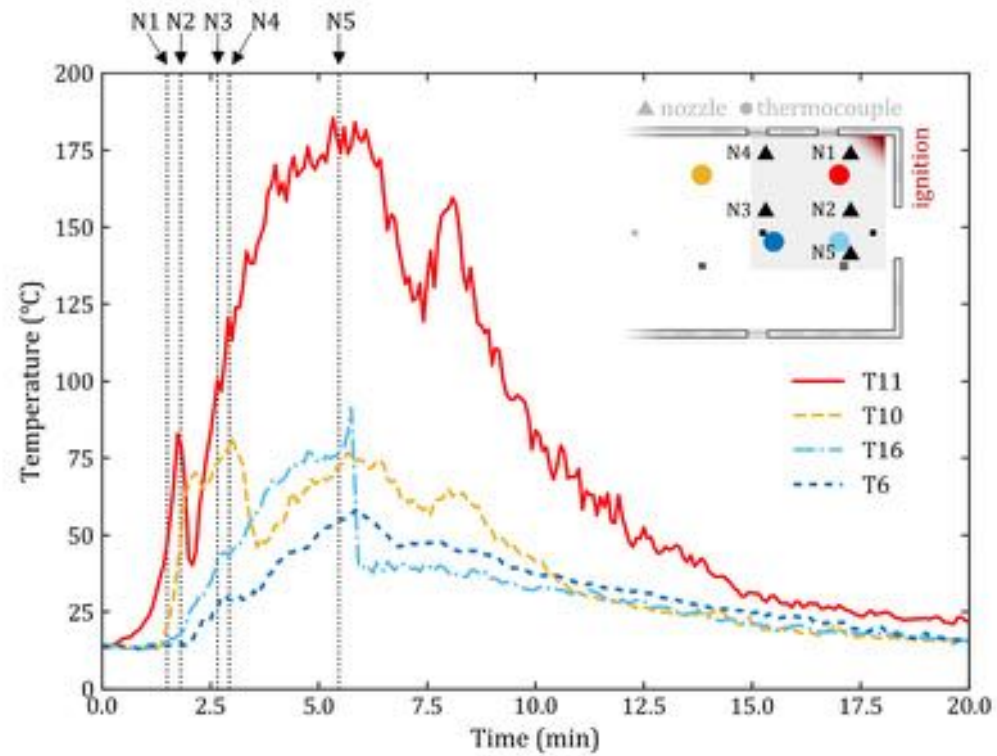
## Abstract

The desire by developers and architects to build mass timber buildings using cross laminated timber (CLT) and glulam has significantly increased globally in the last decade due to its benefits with regards to sustainability as well as other architectural and commercial drivers. This paper presents novel experimental evidence from *CodeRed #02*, the second in a series of large scale fire experiments carried out inside a purpose-built, open-plan compartment to capture fire dynamics in large compartments with exposed timber. The experiment used a continuous wood crib (6 × 29 m) as a controlled movable fuel load. The aim of the *CodeRed #02* experiment was to study the impact of

# CodeRed #03

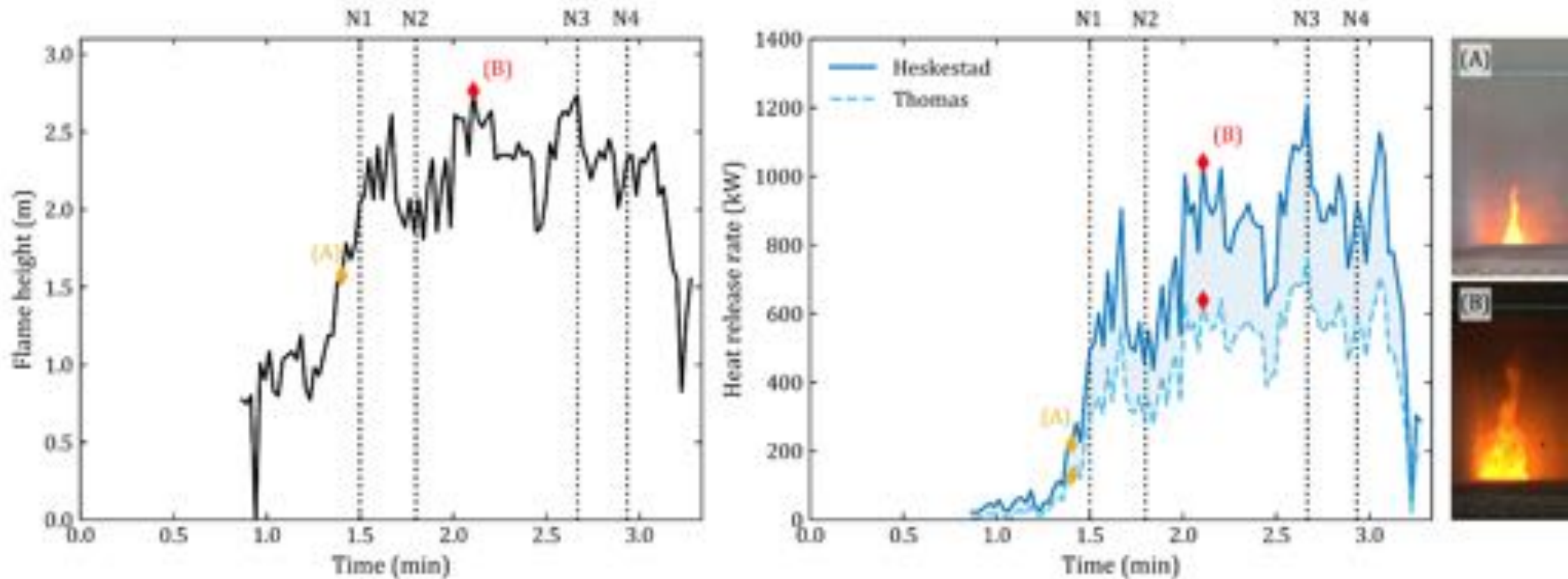
*Effectiveness of water mist system*

# CodeRed #03



Nozzle*	Activation time	Average discharge density
N1	1 min 30 s	3.0 litres/m/min
N2	1 min 48 s	
N3	2 min 40 s	2.93 litres/m/min
N4	2 min 56 s	
N5	5 min 28 s	2.88 litres/m/min

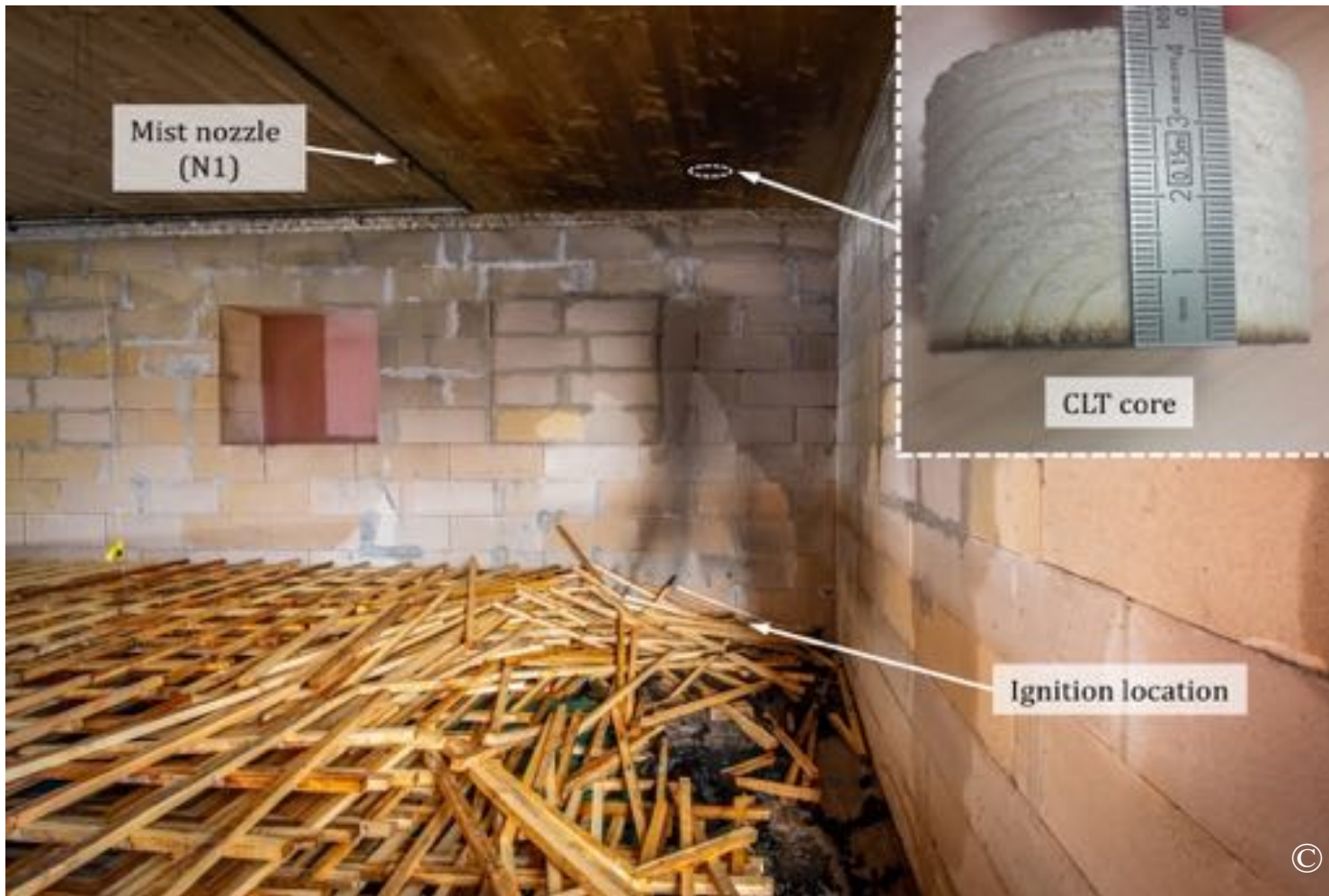
# Flame height and HRR



Peak heat release 762-1205 kW, based on the Thomas and Heskestad methods respectively  
This was achieved 2 min 40 s after ignition, approximately simultaneously with the activation of the third nozzle



# CodeRed #03



### The Effectiveness of a Water Mist System in an Open-plan Compartment with an Exposed Timber Ceiling: CodeRed #03

By P. Katsouras, E. G. Christensen, J. Gale, H. Mitchell, B. Annis, F. Robert, M. Heister, D. Barber, G. Rein, and J. Schult

In recent times, there has been a global surge in the design and construction of mass timber buildings due to their benefits, particularly regarding sustainability. Many of these buildings are proposed to be used in commercial premises with open-plan layouts. As discussed by Rackauskaite et al., [1] compartment fire experiments with exposed timber surfaces published at the time of the authors' review were limited to a compartment area of 84 m<sup>2</sup>. In contrast, open floor office spaces often exceed 1000 m<sup>2</sup>. To address this limitation in research and meet current design needs, researchers conducted a series of full-scale fire experiments in a very large purpose-built compartment of 352 m<sup>2</sup>. To address this limitation in research and meet current design needs, the research team conducted a series of full-scale fire experiments in a very large purpose-built compartment of 352 m<sup>2</sup>. The experiments were performed at CERIB's fire testing facility in France. These experiments aim to capture fire dynamics in large compartments with exposed timber and develop solutions for design [2], [3].

This article presents novel experimental evidence from the third experiment in the series, CodeRed #03. The aim of the first two experiments (CodeRed #01 and #02) were to capture fundamental fire dynamics, while the third experiment was to investigate the effectiveness of a standard water mist suppression system in both limiting fire growth as well as preventing the ignition of an exposed CLT ceiling. Providing an automatic suppression system is a common mitigation measure used in mass timber buildings that, with other protective measures (such as encapsulation, fire-fighting facilities, etc.), aim to address the additional risks introduced by the combustible nature of the structural frame.

#### Experimental Set-up

The facility where the experiment was undertaken is described in detail in [2]. The compartment has internal dimensions 10.27 × 34.27 × 3.1 m with a floor plate area of ~352 m<sup>2</sup>. The CodeRed #03 experiment has several open windows and doors to imitate possible ventilation conditions in an office environment with operable windows during the very early stages of a fire.

The equivalent theoretical fire load that would be present in buildings was replicated by constructing a wood crib in part of the enclosure with a fuel load density of ~570 MJ/m<sup>2</sup> and which covered a floor area of ~50 m<sup>2</sup> (7 m × 7 m). The fuel load density corresponds to the 80% fractile for offices as per PD 6688-1-2:2007 "Background paper to the UK National

# CodeRed #04

*Impact of partial encapsulation*

# MEP considerations



## MEP fixings included

Indicative of Unistrut support spacings expected for commercial office fitout



## Fixing matrix

M8-10 fixings (loaded and unloaded)  
Into bare CLT vs into protected CLT



## Post fire investigation

Saw cut through fixings into CLT

# CodeRed #04



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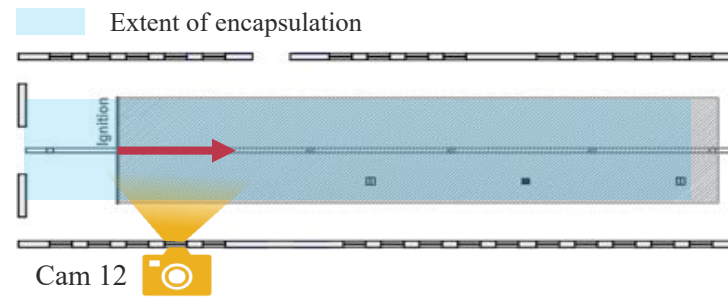
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# CodeRed #04



# Notable events

## Initial fire spread



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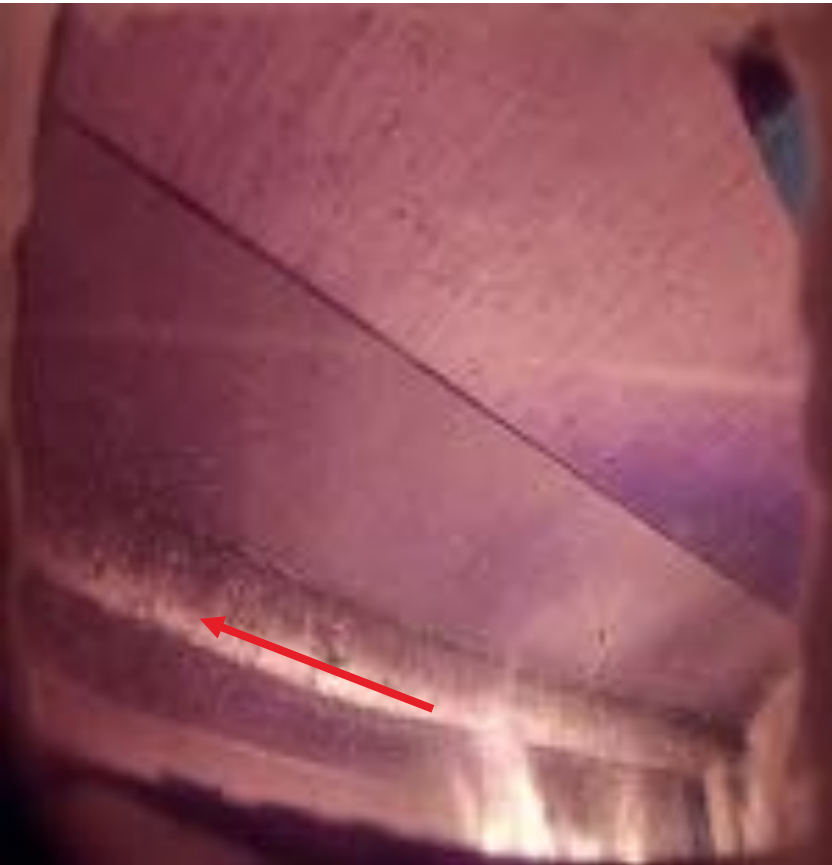
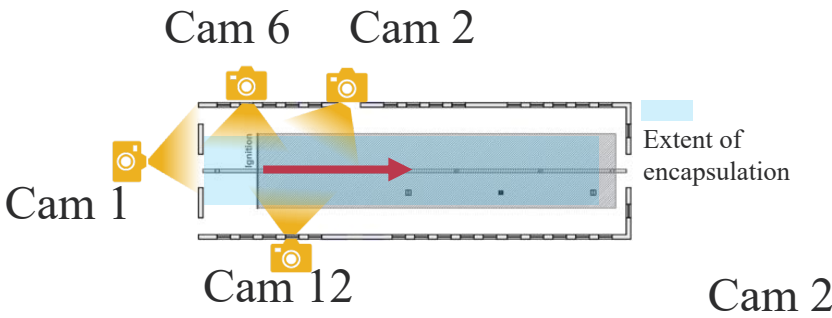


Steady spread of both leading and trailing edge – rapid acceleration post CLT ignition

Note: preliminary results

# Notable events

## CLT ignition



**23 min 52 s**  
 Right side CLT ignites, glowing visible on left side!  
 (started 18.47)



**24 min 57 s**  
 CLT on left side ignites



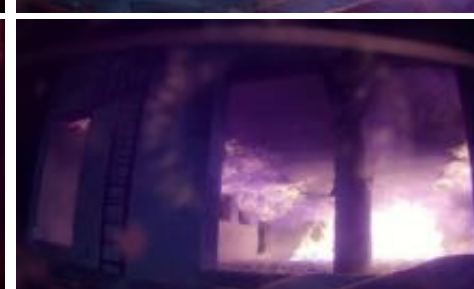
**25 min 54 s**  
 flaming on right side dies down



**27 min 26 s**  
 flaming on left side dies down, as right side grows



**28 min 55 s**  
 left sides grows again





# Peak heat flux and temperatures

- Peak heat fluxes are lower in CodeRed#04 than in #01
- Peak temperatures near the ceiling appear to be similar between experiments
- Peak temperature close to the ground appear to be between those from a non-combustible and fully exposed timber structure.

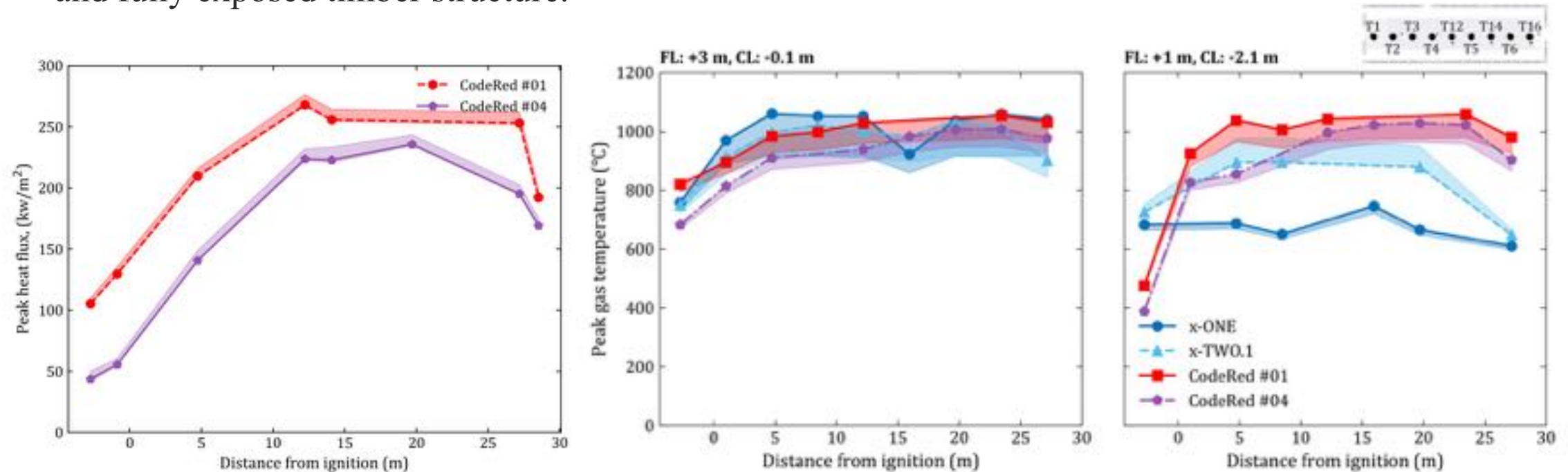
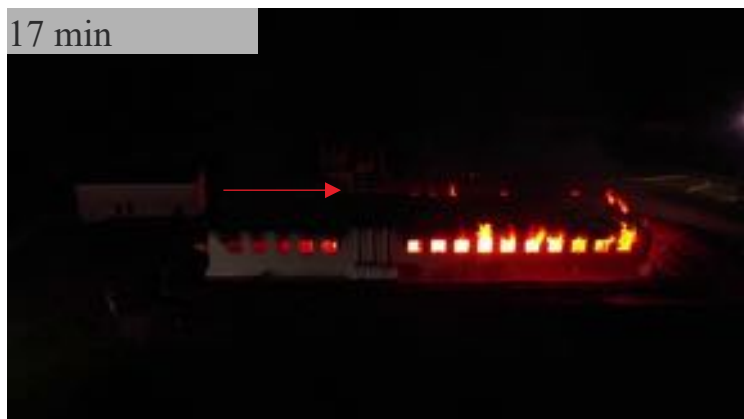


Figure – Peak incident heat flux values measured along the centreline of the compartment near the ceiling.

Figure – Peak temperatures measured along the centreline of the compartment.

CodeRed #01



- 6 min

similar

fire travelled to far end  
 localised external flaming there  
 CodeRed #04 smaller flames  
 as expected due to reduced CLT fire load

+ 5 min

*12 min and 36 min chosen as approx. mid-point  
 of 'peak' external flaming for each experiment*

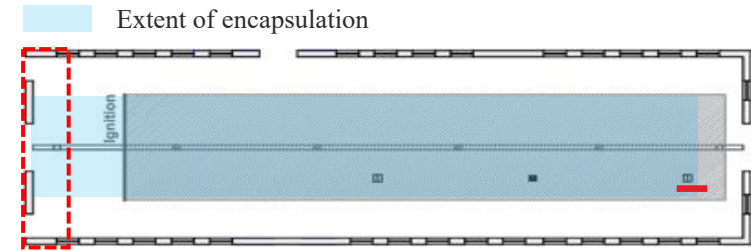
CodeRed #04

# Below encapsulation

Some smouldering occurred below CLT encapsulation.

This is isolated to the first CLT slab.

Linked to location of smouldering near the junction



6th of January, 23 days after the experiment



At the end of encapsulation



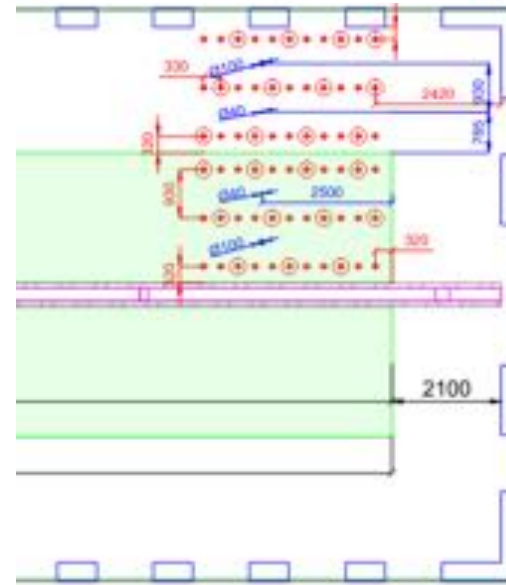
Approximate encapsulation location



# Mechanical fixings

- Included mechanical fixings representative of services hung from ceiling
- Informed by projects currently in concept design
- Half in CLT, half in encapsulated CLT

- Penetration seal
- Mechanical fixing with a load of 27 kg
- Mechanical fixing without loading



# Key issues identified

**These need to be addressed in tall mass timber buildings**

- Fire spread across large areas of exposed timber is fast –
- External flaming and the likelihood that fire spread will occur
- The lower portion of exposed columns can be more vulnerable
- Smouldering will occur in joints and interfaces for days afterwards
- Current compartment fire models are not adequately reflecting fire behaviour in large compartments with exposed CLT



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Thank you and questions

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