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# Analysis of Structures in Fire Using General Structural Analysis Software

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### Predicting steel frame behaviour in fire

- Internal forces arising from localised fires are often detrimental to steel frame structures
- Proprietary FE software (ie SAFIR, Vulcan, LS-Dyna) is expensive and time consuming
- General structural analysis software (Robot, RFEM etc.):
  - Models often easily obtained for a project
  - Lack functionality required
- A workflow create to allow general structural analysis software for steel frame buildings exposed to localised fires
- Limited to relatively low temperature scenarios (localised fires in large open spaces)



### **Workflow Overview**



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# Defining the localised design fire

- Modelled based on equations described in the SFPE Handbook
- Conservatively idealised in a cylindrical shape
- Split into three main geometrical components:
  - Continuous flame
  - Intermittent flame
  - Thermal plume



• Each zone has different parameters to calculate radiative/convective heat transfer

#### **Steel Temperature Model**

- In-house python script based on equations from EN 1993-1-2 for protected and unprotected steel
- Allows temperature of an element to be calculated anywhere in 3D space in relation to design fire



## **Equivalent Stiffness**

• Overestimation of axial force in heated restrained member due to ignoring the reduction in Young's Modulus at elevated temperatures

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for 
$$20^{\circ}C \leq \theta_a < 750^{\circ}C$$
:

$$\Delta l/l = 1.2 \times 10^{-5} \,\theta_{\rm a} + 0.4 \times 10^{-8} \,\theta_{\rm a}^{\,2} - 2.416 \times 10^{-4}$$

### **Equivalent Stiffness**

- Stiffness rapidly decreases at higher temperatures
- Max equivalent temperature taken when actual temperature reaches 500°C (conservative)



### **Maximum Element Temperature and Equivalent Temperature**

- Members split into nodes
- Steel maximum and equivalent temperature calculated at each node
- Average equivalent temperature is used to calculate internal forces and maximum temperature used for member verification
- It should be noted that members heat at different rates and therefore temperatures should be calculated at multiple time steps



#### **Structural Analysis Overview**



## **Connection Design**

- Important to consider connection design for increased axial loads and moments
- Possible to investigate how plastic deformations and bolt hole tolerances assist in dissipating increased forces

$$\label{eq:add} \begin{split} dF_{add} &= dL \ / \ L \times EA \\ dL_{req} &= dF_{add} \ / \ (EA) \times L \end{split}$$

Where:

- $dF_{add}$  additional force in connection above ULS
- $dL_{req}$  change in length of the element
- $L-{\rm length}$  of the element
- A cross sectional area of the element
- E Steel Young's Modulus

# **CASE STUDY:** Typical Waste-to-Energy plant

 Requirement for fire protection (NFPA 850): all steelwork supporting fire-rated walls to be protected to R120





# **CASE STUDY:** Design Fires



# **CASE STUDY:** Heat Transfer

- Zone model (CFAST) used to obtain smoke temperatures
- Temperature calculated for each node





# **CASE STUDY:** Thermo-Structural Analysis

- Equivalent temperature input to RFEM to account for thermally induced forces
- EC3 checks for each member undertaken using maximum temperatures





# **CASE STUDY:** Thermo-Structural Analysis

- Redundancy analysis
- Connection design



# **CASE STUDY:** Results

- Analysis showed partial protection of R60 required
- Recommended to increase section size of some members



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# Thank you for listening!

Any questions?

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